

Simulation Studies on A Cross Flow Plate Fin Heat Exchanger

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Abstract: Compact heat exchangers which were initially developed for the aerospace industries in the 1940s have been considerably improved in the past few years. The main reasons for the good performance of compact heat exchangers are their special design which includes turbulent which in turn use high heat transfer coefficient and resists fouling, and maximum temperature driving force between the hot and cold fluids. Numerous types use special enhancement techniques to achieve the required heat transfer in smaller plot areas and, in many cases, less initial investment. One such type of compact heat exchanger is the Plate-fin heat exchanger. The complexity of compact heat exchanger design equations results from the exchangers unique ability to transfer heat between multiple process streams and a wide array of possible flow configurations. This paper presents the performance evaluation of cross flow plate fin heat exchanger with several different Gas-Liquid systems. Experimental results such as exchanger effectiveness, overall heat transfer coefficients were calculated for the flow systems of Cross flow Heat Exchangers. A steady state model for the outlet temperature of both the cold and hot fluid and overall heat transfer coefficient of a plate-fin cross flow heat exchanger was developed and simulated using MATLAB, which was verified with the experiments conducted.

Key words: Overall heat transfer coefficient, surface effectiveness, exchanger effectiveness, fin effectiveness

INTRODUCTION

Heat Exchanger is process equipment designed for effective transfer of heat energy between two fluids (a hot fluid and a cold fluid). Many types of heat exchangers are used in industry, such as shell and tube, double pipe, compact heat exchangers etc, which vary both in application and design. The choice of heat exchanger type directly affects the process performance and also influences plant size, plant layout, length of pipe runs, and the strength and size of supporting structures. Plate fin heat exchangers form one of the main categories of compact heat exchangers designed to pack a high heat transfer capacity into small volume. Heat transfer is mainly function of surface area; therefore by increasing surface area per unit volume high performance can be obtained with a small size heat exchanger. Performance analysis of cross flow heat exchanger was carried out.^[3] by using air as one of the fluid. An approach to fouling allowances in the design of compact heat exchangers was discussed.^[4] An approximate method for transient behavior of finned tubes cross flow heat exchangers was discussed.^[6] In the present study, experimental investigations were

carried by using miscible systems. Steam is the hot fluid, whereas Water and Acetic acid-Water miscible solution serves as cold fluid. A series of runs were made between steam and water, steam and Acetic acid solution. In addition to, the volume fraction of Acetic acid was varied and the experiment was held. The flow rate of the cold fluid is maintained from 30 lph to 300 lph for Cross flow Heat Exchanger, and the volume fraction of Acetic acid is varied from 10-50%. Experimental results such as exchanger effectiveness, overall heat transfer coefficients were calculated for the flow systems of Cross flow Plate fin Heat Exchanger. A steady state model for the outlet temperature of both the cold and hot fluid and overall heat transfer coefficient of a plate-fin cross flow heat exchanger was developed and simulated using MATLAB, which was verified with the experiments conducted.

MATERIALS AND METHODS

Experimental studies

Experimental setup: The Plate fin heat exchanger, in which heat transfer studies are to be carried out, was fabricated with Aluminum as the material of

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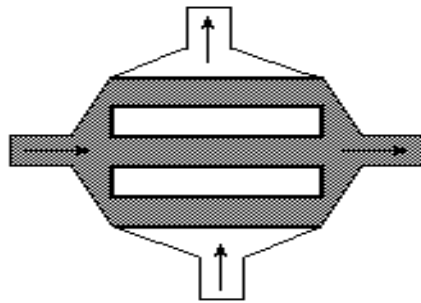


Fig. 1: A cross-flow heat exchanger

construction. The basic element consists of two plates, a strip of corrugated sheet and edge-sealing bars. Here, instead of the edge sealing bars, the flat plate was folded on both sides thus providing an enclosure to the corrugations. The flat plates are termed as Primary surface and the corrugations as 'secondary surface'. The corrugations were welded to the flat plates. Figure 1 shows the schematic of cross flow plate-fin exchanger.

Experimental procedure: The inlet temperature (t_i) of the cold fluid is measured. The pump is operated and the required water or Acetic acid water mixture flow rate is fixed using the valve. The Steam generator is switched on and the steam inlet temperature (T_i) is set to a constant value. The steam flow rate is controlled by the ball valve. As the fluid flow starts on the both sides the phenomenon of heat transfer takes place between hot and cold fluids through the walls of the Tubes. The flow system is allowed to attain steady state. The outlet temperatures of condensate (T_o) and the cold fluid (t_o) are measured. The condensate flow rate is measured at the exit of the Shell. Then the flow rate of the cold fluid is varied and the above procedures are repeated

Experimental observations: Experiments were carried out on five systems having different compositions of Acetic acid and water according to the procedure. The observations are tabulated in the Table 1, 2.

Fin effectiveness, Surface effectiveness, Exchanger effectiveness, the film coefficients for both hot and cold fluids, Overall heat transfer coefficient and NTU calculations for the above observed readings are given in the Table 3, 4 respectively.

Modeling and simulation: A lumped parameter model for the cross flow heat exchanger is derived from heat balance and it is simulated using MATLAB. A physical model is developed by dimensional analysis followed by least square curve fitting experimental data.

Table 1: Steam vs water

Volumetric Flow Rate of Cold fluid (gpm)	Fluid Temperatures (°C)			
	t_{ci}	t_{co}	t_{hi}	t_{ho}
0.44	29	69.5	112	99.5
0.75	29	61.5	112	99.5
1.28	29	56.0	112	99.5
2.43	29	45.0	112	99.5
3.48	29	38.5	112	99.5
4.56	29	37.0	112	99.5
4.68	29	36.5	112	99.5
6.20	29	35.5	112	99.5
6.64	29	35.0	112	99.5
7.20	29	33.5	112	99.5

Table 2: Steam vs 10% acetic acid

Volumetric Flow Rate of Cold fluid (gpm)	Fluid Temperatures (°C)			
	t_{ci}	t_{co}	t_{hi}	t_{ho}
0.7	29	59.0	112	99.5
1.0	29	53.0	112	99.5
1.3	29	49.0	112	99.5
1.5	29	48.0	112	99.5
2.0	29	44.5	112	99.5
2.2	29	42.5	112	99.5
2.5	29	41.0	112	99.5
2.7	29	39.5	112	99.5
3.0	29	38.5	112	99.5
3.5	29	36.5	112	99.5
4.0	29	35.5	112	99.5
4.5	29	35.0	112	99.5

Mathematical modeling:

$$t_o = \frac{(T_i + T_o) + t_i(a-1)}{a+1} \tag{1}$$

$$T_o = \frac{(T_i(ab+b-a)) + (t_i(2a))}{a+b+ab} \tag{2}$$

Equation 1 and 2 represent the required mathematical model for the tube outlet temperature of the cold fluid t_o and the outlet temperature of the hot fluid T_o respectively.

Physical Modeling: The physical model equation was developed using dimensional analysis followed by least square curve fitting experimental data as follows:

$$St = 0.332 (Re)^{-0.5} (Pr)^{0.667} (\mu)^{0.997}$$

Simulation: The models derived above are simulated using MATLAB. Equation 1 and 2 are used to predict the outlet temperature of the cold and hot fluid, respectively. Simulation is done for all flow rates and 10 % Acetic acid for which experiments were done and are plotted in Fig. 2 to along with the experimental values.

Table 3: Steam-water system

Cold fluid (Water)		Hot fluid (Steam)			Heat transfer coefficient (W/m ² K)						Surface Effectiveness (%)		Fin Effectiveness (%)		Exchanger Effectiveness (%)
t _{ci} (°C)	t _{co} (°C)	M _c (kg/hr)	t _{hi} (°C)	t _{ho} (°C)	M _h (kg/hr)	Hot fluid ho	Cold fluid hi	Overall U	C*	NTU	Hot fluid ηs1	Cold fluid ηs2	Hot fluid ηf1	Cold fluid ηf2	ε
29	69.5	26.063	112	99.5	189.56	294.295	318.274	148.677	0.301	3.25	97.36	97.10	96.24	95.95	89.80
29	61.5	44.536	112	99.5	261.35	299.110	455.444	174.612	0.373	2.24	97.25	95.92	96.18	94.32	80.10
29	56.0	76.132	112	99.5	360.26	294.577	567.749	187.161	0.462	1.40	97.29	95.00	96.23	93.04	65.15
29	45.0	144.88	112	99.5	375.74	276.527	768.300	195.925	0.843	0.71	97.45	93.43	96.46	90.86	42.76
29	38.5	207.75	112	99.5	258.69	300.932	941.775	218.866	0.613	0.98	97.24	92.13	96.16	89.05	52.15
29	37.0	272.29	112	99.5	270.99	272.622	1191.91	213.174	0.484	0.92	97.48	90.36	96.50	86.60	52.32
29	36.5	279.48	112	99.5	260.76	310.359	1188.11	235.460	0.454	1.06	97.15	90.44	96.04	86.64	56.98
29	35.5	370.38	112	99.5	232.30	350.476	1184.77	257.732	0.305	1.30	96.81	90.42	95.56	86.67	66.17
29	35.0	396.63	112	99.5	250.50	336.081	1184.97	249.813	0.306	1.73	96.93	90.42	95.73	86.67	62.88
29	33.5	430.19	112	99.5	185.46	298.426	1225.05	229.832	0.210	1.45	97.25	90.15	96.18	86.29	71.86

Table 4: 10% acetic acid-water solution

Cold fluid (Water)		Hot fluid (Steam)			Heat transfer coefficient (W/m ² K)						Surface Effectiveness (%)		Fin Effectiveness (%)		Exchanger Effectiveness (%)
t _{ci} (°C)	t _{co} (°C)	M _c (kg/hr)	t _{hi} (°C)	t _{ho} (°C)	M _h (kg/hr)	Hot fluid ho	Cold fluid hi	Overall U	C*	NTU	Hot fluid ηs1	Cold fluid ηs2	Hot fluid ηf1	Cold fluid ηf2	ε
29	59.0	41.833	112	99.5	208.07	323.241	465.378	184.196	0.417	2.65	97.05	95.85	95.89	94.22	82.73
29	53.0	59.899	112	99.5	238.39	354.732	507.656	201.126	0.521	2.03	96.88	95.51	95.67	93.73	73.63
29	49.0	77.993	112	99.5	258.67	329.924	560.069	199.920	0.625	1.54	97.03	95.06	95.87	93.13	64.26
29	48.0	90.027	112	99.5	283.65	310.793	592.382	196.851	0.658	1.32	97.21	94.88	96.11	92.88	59.38
29	44.5	120.20	112	99.5	308.94	302.882	670.823	201.207	0.806	1.01	97.38	94.17	96.35	91.89	49.89
29	42.5	132.32	112	99.5	296.19	300.378	701.927	202.839	0.926	0.92	97.35	93.95	96.32	91.58	46.04
29	41.0	150.58	112	99.5	299.57	298.823	758.716	206.611	0.958	0.86	97.32	93.55	96.27	91.03	43.95
29	39.5	162.59	112	99.5	283.01	300.737	762.923	207.468	0.840	0.91	97.28	93.48	96.21	90.92	47.06
29	38.5	180.73	112	99.5	284.60	307.148	765.471	210.970	0.760	0.93	97.27	93.44	96.09	90.88	48.42
29	36.5	211.01	112	99.5	262.29	321.711	861.614	224.719	0.600	1.07	97.07	92.89	95.92	90.12	54.75
29	35.5	241.26	112	99.5	259.86	331.528	929.630	234.192	0.50	1.12	96.98	92.35	95.81	89.29	57.60

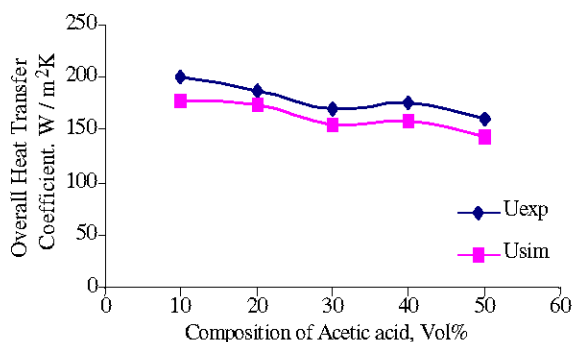


Fig. 2: Overall Heat Transfer Coefficient Vs Vol. flow rate of Cold fluid and composition of cold fluid

RESULTS AND DISCUSSIONS

The effects of different input variables on output variable are discussed in detail in the following sections.

Overall heat transfer coefficient for CFHE: As the volumetric flow rate of the tube side fluid is increased from 60 lph to 300 lph, the overall heat transfer coefficient increased from 184.196 to 234.192 W/(m² K). For the same volumetric flow rates, the simulated

values varied from 176.329 to 193.429 W/m²K respectively, i.e., almost same as experimental values.

Shell outlet temperature for CFHE: For the flow rate increments from 30 lph to 300 lph, the outlet temperature of the shell side fluid remains constant as 99.5°C, whereas the simulated values were 95 to 89°C respectively.

Tube outlet temperature for CFHE: For the flow rate increments from 30 lph to 300 lph, the outlet temperature of tube side fluid varied from 59 to 35.5°C, whereas the simulated values were 49 to 35°C respectively.

The results for the other compositions were similar to that obtained from the one considered here as the reference. From the above comparisons it can be said that the mathematical model developed for the system is very close. The deviation in shell outlet temperature may be because of the assumption of negligible condensation.

CONCLUSION

Experiments were conducted on a plate-fin type cross flow heat exchanger with different cold side flow

rates and different compositions of cold fluid. The effect of these parameters on the shell outlet temperature, tube outlet temperature and overall heat transfer coefficients were studied. It was found that cold fluid outlet temperature decreases and the overall heat transfer coefficient increases with increases with increase in flow rate of cold fluid. Also the outlet temperature of cold fluid decreases and overall heat transfer coefficient increases with increase in composition of more heat capacity fluid. The overall effectiveness of heat exchanger was found to decrease with increase in temperature and increasing with increase in composition of high heat capacity fluid. A mathematical model of this system is developed, simulated using MATLAB and compared with the experimental values and it was found that the model predictions were close to experimental values. Finally a correlation for the calculation of film heat transfer coefficient is developed which can be used for both the cold and hot side.

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